Table 1: HST (FOS and GHRS) quasar Lyman-α emission line spectra.

Name (NED)	z (NED)	Instrument	Aperture	Grating	S/N (mean)	Comments on spectra and fits.
MRK 0335	0.026	FOS	B-3	H13	16.2	Fit with free line centers flags a large number of pixels as "emission" features.
FAIRALL 0009	0.047	FOS	B-3	H13	10.8	Excluded due to non-convergence of feature detection.
UGC 00545	0.061	FOS	B-3	H13	25.6	Excluded due to non-convergence of feature detection.
UGC 11763	0.063	HRS	LSA	G140L	20.5	Excluded due to non-convergence of feature detection.
MR 2251-178	0.064	FOS	B-3	H13	14.3	Excluded due to non-convergence of feature detection.
TON 1187	0.079	FOS	B-3	H13	11.0	Feature detection did not converge for red-side fit with zero shift.
MRK 0478	0.079	FOS	B-3	H13	11.6	Excluded due non-convergence of feature detection (all fits).
PG 1211+143	0.081	FOS	B-3	H13	11.2	Excluded due to non-convergence of feature detection.
PG 1211+143	0.081	HRS	LSA	G140L	26.7	Excluded due to non-convergence of feature detection.
SDSS J12305003+0115226	0.117	HRS	LSA	G140L	25.0	Excluded due to feature detection non-convergence (and many absorption features).
SBS 1626+554	0.133	FOS	B-3	H13	10.5	Strong absorption feature at line center.
PG 0026+129	0.142	FOS	B-3	H13	15.0	Full fit spuriously excludes a large region on red side as absorption, but fits well on the blue side of the line.
PG 1114+445	0.144	FOS	B-3	H13	12.7	Excluded due to non-convergence of feature detection.
3C 273	0.158	FOS	C-2	H13	20.9	
3C 273	0.158	FOS	B-2	H13	19.9	
3C 273	0.158	FOS	B-3	H13	17.6	
3C 273	0.158	FOS	A-1	H13	17.0	
3C 273	0.158	FOS	B-1	H13	18.1	
PG 1322+659	0.168	FOS	B-3	H13	18.0	Full fit excludes a large section of blue side contaminated with ISM lines.
PG 1116+215	0.176	FOS	C-2	H13	15.9	
[HB89] 1427+480	0.221	FOS	B-3	H13	12.8	Absorption feature in blue wing of the line (flagged in full fit).
PG 0953+414	0.234	FOS	C-2	H13	11.1	Absorption feature at line center.
[HB89] 1156+213	0.349	FOS	B-3	H19	10.7	
PG 1049-005	0.360	FOS	C-2	H19	13.6	Excluded due to bad blue edge of spectrum.
[HB89] 1425+267	0.366	FOS	B-3	H19	12.5	Strong absorption line just blueward of line center.
HS 0624+6907	0.370	FOS	B-2	H19	17.2	
SBS 1704+608	0.372	FOS	C-2	H19	13.9	Excluded due to bad blue edge of spectrum.
[HB89] 1543+489	0.400	FOS	B-3	H19	27.4	Highly asymmetric profile. Red-side fit with median shifts failed to converge.
3C 215	0.412	FOS	A-1	H19	11.7	
LBQS 1230+0947	0.414	FOS	A-1	H19	10.3	
[HB89] 1049+616	0.421	FOS	C-1	L15	13.4	
[HB89] 2308+098	0.433	FOS	B-3	H19	17.4	
PG 0003+158	0.451	FOS	C-2	H19	19.9	

The name and redshift z are from NED.

Continued on next page.

Table 1: Quasar spectra. – continued from previous page.

Name (NED)	z (NED)	Instrument	Aperture	Grating	S/N (mean)	Comments on spectra and fits.
FBQS J0745416+314256	0.461	FOS	C-2	H19	13.3	
[HB89] 2112+059 NED01	0.466	FOS	C-2	H19	13.0	
SBS 1259+593	0.478	FOS	C-2	H19	16.1	Poorly constrained very narrow component in all red-side fits.
[HB89] 2128-123	0.501	FOS	C-2	H19	19.9	Full profile fit flags red side of the Ly-alpha line core.
[HB89] 1130+111	0.510	FOS	C-2	H19	10.6	Excluded due to bad blue edge.
[HB89] 0850+440	0.514	FOS	C-2	H19	10.8	
FBQS J0958209+322402	0.530	FOS	C-2	H19	10.9	Missing some flux values at line center (flagged during coadding).
[HB89] 0454-220	0.533	FOS	B-3	H19	25.1	Excluded due to non-convergence of feature detection.
TON 0156	0.549	FOS	B-3	H19	31.6	Excluded due to problems with coadded spectrum.
[HB89] 0015+162	0.553	FOS	B-3	H19	12.5	
PG 1333+176	0.553	FOS	C-2	H19	12.3	Excluded due to bad blue edge of spectrum.
3C 334	0.555	FOS	C-2	H19	15.0	
NGC 2841 UB3	0.556	FOS	C-2	H19	14.3	
[HB89] 1136-135	0.558	FOS	C-2	H19	11.5	Red-side fit spuriously flagged some of narrow component.
[HB89] 0405-123	0.573	FOS	C-2	H19	18.2	
[HB89] 0439-433	0.593	FOS	C-2	H19	14.0	Region of red side flagged as emission in full-profile fit.
FBQS J1010275+413238	0.612	FOS	C-2	H19	19.9	
3C 095	0.616	FOS	C-2	H19	17.2	
PG 0044+030	0.623	FOS	C-2	H19	10.8	
[HB89] 1104+167	0.632	FOS	C-2	H19	17.9	
[HB89] 2243-123	0.632	FOS	C-2	H19	17.2	
3C 263	0.646	FOS	A-1	H19	10.2	
3C 263	0.646	FOS	C-2	H19	14.2	
3C 057	0.669	FOS	B-2	H19	25.2	
[HB89] 2344+092	0.677	FOS	C-2	H19	12.5	Full fit flags edges of the narrow component as emission features.
[HB89] 0923+392	0.695	FOS	A-1	H19	21.1	
[HB89] 2352-342	0.702	FOS	C-2	H19	15.8	Red edge of narrow component is flagged in red-side fits.
[HB89] 1354+195	0.720	FOS	C-2	H19	11.4	
FBQS J1159+2914	0.729	FOS	B-3	H19	13.5	Excluded due to poor signal-to-noise, weak emission lines.
[HB89] 1637+574	0.751	FOS	A-1	H19	10.9	
[HB89] 1538+477	0.772	FOS	C-2	H19	21.7	Several absorption features on red and blue side.
2MASSi J1003067+681316	0.773	FOS	C-2	H19	12.3	Poorly constrained narrow component in red-side fits.
3C 110	0.775	FOS	B-3	H19	12.1	

The name and redshift z are from NED.

Continued on next page.

Table 1: Quasar spectra. – continued from previous page.

Name (NED)	z (NED)	Instrument	Aperture	Grating	S/N (mean)	Comments on spectra and fits.
FBQS J1253175+310550	0.780	FOS	B-3	H19	28.9	
LBQS 0102-2713	0.780	FOS	B-3	H19	27.4	
3C 286	0.849	FOS	A-1	L15	13.2	
3C 4543	0.859	FOS	C-2	H27	12.0	Narrow component poorly constrained in all red-side fits.
3C 4543	0.859	FOS	A-1	H27	13.4	
[HB89] 0107-156	0.861	FOS	B-3	H27	16.7	Narrow component poorly constrained in red-side fits.
[HB89] 1252+119	0.873	FOS	C-2	H27	12.5	
LBQS 0253-0138	0.879	FOS	A-1	H27	10.2	
[HB89] 2340-036	0.892	FOS	C-2	H27	16.0	Lots of bad pixels. Full fit has unconstrained emission component on red side of line.
[HB89] 0954+556	0.896	FOS	A-1	H27	10.9	
[HB89] 2216-038	0.901	FOS	A-1	H27	14.7	
PKS 0823-223	0.910	FOS	B-3	H27	15.5	Excluded due to lack of visible emission lines in spectrum.
3C 336	0.927	FOS	B-3	H27	13.9	ISM absorption line in center of Ly-alpha line. Other prominent absorption features.
FBQS J1409239+261821	0.940	FOS	C-2	H27	15.6	Excluded due to weak emission lines.
SBS 1340+606	0.964	FOS	A-1	H27	12.7	Excluded due to strong absorption features (blue- and red-side).
3C 094	0.965	FOS	A-1	H27	10.9	Excluded due to strong absorption lines (red and blue side).
TON 0157	0.971	FOS	B-3	H27	15.6	Negative narrow component in red-side fit.
SBS 1148+549	0.975	FOS	A-1	H27	15.2	Very broad, blended emission lines.
[HB89] 2145+067	0.990	FOS	C-2	H27	10.9	Highly asymmetrical profile.
[HB89] 0355-483	1.016	FOS	A-1	H27	12.0	Narrow component poorly constrained in red-side fits.
TON 0153	1.022	FOS	C-2	H27	16.3	
PG 1254+047	1.025	FOS	C-2	H27	15.6	Narrow component poorly constrained in red-side fit. Red-side fit with median shifts failed to converge. Very broad blended emission lines.
PG 1248+401	1.033	FOS	B-2	H27	16.1	
[HB89] 2230+114	1.037	FOS	A-1	H27	13.2	
LBQS 1229-0207	1.043	FOS	C-1	H27	17.8	
[HB89] 2302+029	1.044	FOS	B-3	H27	25.0	Unusual line shape and lots of absorption features.
SBS 1317+520	1.061	FOS	A-1	H27	12.5	
[HB89] 1718+481	1.084	FOS	C-2	H27	27.5	Several absorption features and many bad pixels.
[HB89] 0024+224	1.119	FOS	C-2	H27	11.9	Narrow absorption in line center.
PG 1352+011	1.127	FOS	C-2	H27	14.0	Several moderate-width absorption features. Poorly constrained very narrow component in blue-side fits.
PG 1206+459	1.163	FOS	C-2	H27	15.5	Some narrow absorption features.
PG 1338+416	1.214	FOS	C-2	H27	12.3	Excluded due to prominent IGM absorption features.

The name and redshift z are from NED.

Continued on next page.

Table 1: Quasar spectra. – continued from previous page.

Name (NED)	z (NED)	Instrument	Aperture	Grating	S/N (mean)	Comments on spectra and fits.
PG 0946+301	1.221	FOS	B-3	H27	20.7	Excluded due to strong, broad absorption features.
[HB89] 1038+064	1.270	FOS	B-2	H27	19.6	Several narrow absorption lines.
PG 1241+176	1.273	FOS	C-2	H27	20.7	Some narrow blue-side absorption features.
PG 1008+133	1.289	FOS	C-2	H27	17.4	Missing red-side fit with median shifts due to non-convergence of feature detection. Many narrow absorption features.
[HB89] 1634+706	1.334	FOS	C-2	H27	45.6	Excluded due to non-convergence of feature detection.
[HB89] 0454+039	1.345	FOS	C-1	H27	17.0	Excluded due to non-convergence of feature detection.
[HB89] 0454+039	1.345	FOS	B-3	H27	14.3	Lots of narrow absorption features.
FBQS J1259487+342322	1.375	FOS	C-2	H27	12.8	Strong narrow absorption feature just redward of line center.
[HB89] 0302-223	1.409	FOS	B-1	H27	23.5	Narrow component poorly constrained in red-side fits.
[HB89] 0957+561	1.414	FOS	B-1	H27	44.6	Excluded due to strong absorption features (red and blue side).
3C 298	1.437	FOS	B-3	H27	21.3	Excluded due to strong, broad absorption lines (red and blue side).
[HB89] 0232-042	1.440	FOS	B-2	H27	24.0	
SDSS J12184047+5015434	1.456	FOS	A-1	H27	24.3	Excluded due to missing flux values.
UM 425	1.462	FOS	B-2	H27	19.7	Excluded due to prominent broad absorption lines (red and blue side).
[HB89] 1630+377	1.476	FOS	B-1	H27	28.6	
PG 0117+213	1.493	FOS	B-2	H27	19.6	Many narrow absorption features. Red-side fit has a poorly-behaved narrow component.
[HB89] 0743-673	1.510	FOS	C-2	H27	22.0	Large section of line spuriously flagged by feature detection in full fit. Blue side of fit still good.
LBQS 1026-0045B	1.531	FOS	B-3	H27	22.6	Excluded due to misaligned sub-spectra.
[HB89] 1115+080	1.735	FOS	B-2	H40	22.5	Excluded due to absorption features (in both Ly-alpha and NV).
CTS 0286	2.545	FOS	B-1	L65	23.1	Excluded due to high redshift and low resolution.
[HB89] 1413+117	2.558	FOS	B-1	H40	20.5	Excluded due to broad absorption features.
MAPS-NGP O_382_0380226	3.620	FOS	B-2	H57	24.2	Excluded due to high blue-side IGM absorption.

The name and redshift z are from NED.

Table 3: Best-fit spectral parameters from fits to the full line profile.

Name	Inst. Grat. Ap.	$\sigma_{L\alpha 0}$ (Å)	$a_{L\alpha 0}$ (a_p)	$v_{L\alpha 0}$ (km/s)	$\sigma_{L\alpha 1}$ (Å)	$a_{L\alpha 1}$ (a_p)	$v_{L\alpha 1}$ (km/s)	σ_{NV} (Å)	a_{NV} (a_p)	v_{NV} (km/s)	p	a_p (flux)	χ^2/ν prof.	χ^2/ν cont.	ν prof.	ν cont.
MRK 0335	FOS H13 B-3	2.13	8.48	100	9.18	2.80	-258	4.76	0.98	24	-1.09	76.2	1.24	0.88	199	177
SBS 1626+554	FOS H13 B-3	4.76	2.26	-518	17.1	1.42	-94	6.63	0.49	-156	-1.35	21.8	1.27	1.24	326	217
PG 0026+129	FOS H13 B-3	3.29	12.22	1824	14.9	1.04	694	5.22	0.92	1108	-1.06	19.1	1.20	1.26	311	199
3C 273	FOS H13 A-1	4.48	1.44	-557	16.9	0.68	-169	6.44	0.19	283	-1.30	270	0.76	0.79	372	204
3C 273	FOS H13 B-3	4.25	1.57	-631	17.1	0.68	-135	7.58	0.16	102	-1.17	268	1.14	1.08	354	204
3C 273	FOS H13 B-1	4.18	1.58	-610	16.7	0.67	-491	7.62	0.21	39	-1.21	280	1.15	1.04	352	203
3C 273	FOS H13 C-2	4.14	1.46	-524	15.2	0.71	-523	7.51	0.23	66	-1.34	280	1.03	0.88	317	160
3C 273	FOS H13 B-2	4.1	1.58	-644	16.6	0.70	-250	7.47	0.19	245	-1.39	274	0.83	0.82	355	203
PG 1322+659	FOS H13 B-3	3.48	3.84	-220	11.5	2.46	-1007	5.03	0.93	-308	-1.25	9.2	2.63	1.51	279	194
PG 1116+215	FOS H13 C-2	4.41	1.29	-336	14.2	1.02	-683	6.96	0.48	115	-2.38	58.7	0.88	0.58	362	219
[HB89] 1427+480	FOS H13 B-3	3.54	3.81	213	13.5	1.61	-457	6.4	0.56	309	-1.10	7.8	1.32	1.08	350	110
PG 0953+414	FOS H13 C-2	3.76	3.57	-270	14.9	1.85	-112	5.03	0.68	225	-0.75	16.6	1.35	0.69	396	110
[HB89] 1156+213	FOS H19 B-3	4.62	3.03	-510	17.9	1.57	-1780	7.05	0.56	-470	-1.30	3.15	0.87	0.78	248	156
[HB89] 1425+267	FOS H19 B-3	5.29	0.91	2228	14.4	2.48	-1700	4.97	0.61	775	-1.87	4.01	1.63	0.90	271	185
HS 0624+6907	FOS H19 B-2	4.58	4.13	-786	13.1	2.27	-1365	7.74	1.42	-823	-1.30	15	0.90	0.76	252	133
[HB89] 1543+489	FOS H19 B-3	2.79	1.86	-307	13.7	2.11	-1578	7.11	0.99	-964	-1.23	5.53	1.55	0.99	273	149
3C 215	FOS H19 A-1	2.98	2.91	-498	11.3	4.07	192	7.03	0.76	1019	-3.38	0.929	0.65	0.54	339	197
LBQS 1230+0947	FOS H19 A-1	4.95	2.88	424	13.7	2.40	628	5.33	1.44	830	-0.94	5.86	1.11	1.33	337	175
[HB89] 1049+616	FOS L15 C-1	8.51	0.94	88	23.2	0.86	2733	-0.0497	1.23	967	-2.21	5.74	0.98	0.68	61	39
[HB89] 2308+098	FOS H19 B-3	3.9	1.27	-130	11.8	1.11	-114	7.68	0.49	263	-4.20	7.73	0.71	0.57	330	197
PG 0003+158	FOS H19 C-2	2.44	2.67	-229	10.4	2.09	-315	8.17	0.45	-380	-2.93	13.1	1.28	0.51	327	202
FBQS J0745416+314256	FOS H19 C-2	2.53	1.41	-634	10.8	1.73	-596	8.99	0.50	-951	-4.11	6.86	0.84	0.63	350	214
[HB89] 2112+059 NED01	FOS H19 C-2	3.02	1.34	-1534	18.2	1.20	25	1.51	-0.06	409	-3.09	6.97	0.97	0.59	351	181
SBS 1259+593	FOS H19 C-2	4.57	-0.20	463	17.4	0.83	-879	0.806	-0.10	-43	-2.69	12.6	0.76	0.85	353	216
[HB89] 2128-123	FOS H19 C-2	5.6	3.14	-114	22.8	1.39	1563	0.885	-0.16	1696	-1.30	8.66	1.76	1.88	226	178
[HB89] 0850+440	FOS H19 C-2	3.31	1.10	-26	8.84	1.09	-1100	7.87	0.44	-717	-4.41	5.48	0.43	0.59	341	191
FBQS J0958209+322402	FOS H19 C-2	4.38	0.68	-676	14.7	0.50	-487	7.05	0.24	-124	-3.07	5.47	0.32	0.61	337	224
[HB89] 0015+162	FOS H19 B-3	4.26	2.28	-720	22.7	0.99	117	3.29	0.36	-752	-2.22	0.48	0.98	1.09	346	228
3C 334	FOS H19 C-2	3.27	0.97	-282	16.7	0.95	-478	8.47	0.13	663	-3.85	6.37	0.89	1.01	350	227
NGC 2841 UB3	FOS H19 C-2	3.35	0.71	-841	13	1.00	-1645	7.16	0.51	-1001	-2.78	6.73	1.00	0.98	352	211
[HB89] 1136-135	FOS H19 C-2	1.98	3.40	-495	9.08	2.13	-209	6.4	0.49	-254	-3.69	5.53	1.29	0.92	352	230
[HB89] 0405-123	FOS H19 C-2	2.52	2.56	-213	11.2	1.98	-51	5.92	0.65	97	-1.88	16.6	1.32	0.86	336	210
[HB89] 0439-433	FOS H19 C-2	2.6	3.54	-132	15.7	1.00	-471	6.2	0.29	493	-3.56	4.32	1.39	0.86	340	224

See end of table for explanation of columns. Continued on next page.

Table 3: Parameters from full-profile fits – continued from previous page.

Name	Inst. Grat. Ap.	$\sigma_{\mathrm{L}\alpha 0}$ (Å)	$a_{\mathrm{L}\alpha 0}$ (a_{p})	$v_{\mathrm{L}\alpha 0}$ (km/s)	$\sigma_{\mathrm{L}\alpha 1}$ (Å)	$a_{\mathrm{L}\alpha 1}$ (a_{p})	$v_{\mathrm{L}\alpha 1}$ (km/s)	σ_{NV} (Å)	a_{NV} (a_{p})	v_{NV} (km/s)	p	a_{p} (flux)	χ^2/ν prof.	χ^2/ν cont.	ν prof.	ν cont.
FBQS J1010275+413238	FOS H19 C-2	3.2	2.98	-67	12.9	2.19	-289	5.91	0.86	209	-2.48	6.97	2.09	1.46	338	200
3C 095	FOS H19 C-2	10.7	0.71	-40	26.1	0.45	3087	0.277	-0.03	1818	-2.44	10.1	0.96	1.05	355	237
PG 0044+030	FOS H19 C-2	4.11	1.66	-495	10.8	1.38	-2393	12.5	1.02	-2019	-3.27	4.38	0.69	0.62	390	238
[HB89] 2243-123	FOS H19 C-2	2.47	3.02	-1164	11.9	1.53	-925	7.11	0.36	-528	-3.51	5.35	1.69	0.88	392	239
[HB89] 1104+167	FOS H19 C-2	2.06	1.80	-571	9.25	2.42	-260	9.77	0.79	-962	-2.59	8.39	1.22	1.22	365	239
3C 263	FOS H19 A-1	3.34	3.48	-120	13.6	1.73	250	4.58	0.53	328	-1.58	6.3	1.22	1.16	395	242
3C 263	FOS H19 C-2	2.67	2.88	-309	11.5	1.81	-211	6.2	0.49	622	-2.19	7.62	1.68	0.68	374	240
3C 057	FOS H19 B-2	6.87	1.46	66	10.9	0.50	-4478	7.53	0.56	-266	-1.21	6.85	2.53	1.37	376	235
[HB89] 2344+092	FOS H19 C-2	2.52	5.04	-1037	15.2	1.19	-1709	6.7	0.48	-983	-3.12	4.26	1.42	1.23	347	237
[HB89] 0923+392	FOS H19 A-1	5.18	2.23	591	18.3	1.34	1163	5.67	0.16	779	-0.02	4.33	0.97	1.00	385	189
[HB89] 2352-342	FOS H19 C-2	1.62	2.91	703	12.8	2.27	85	4.84	0.49	940	-2.40	4.89	1.97	0.90	339	227
[HB89] 1354+195	FOS H19 C-2	2.04	4.16	-208	10.3	1.90	-175	5.88	0.51	-47	-3.58	4.16	1.54	0.89	414	160
[HB89] 1637+574	FOS H19 A-1	3.53	2.09	-84	13	1.10	135	6.35	0.48	191	-1.50	3.04	1.16	0.87	422	128
[HB89] 1538+477	FOS H19 C-2	5.92	1.47	-283	15.8	1.96	-148	6.55	0.33	917	-1.10	5.82	2.42	1.80	288	112
2MASSI J1003067+681316	FOS H19 C-2	5.19	0.42	-980	16.4	0.59	-2850	8.19	0.64	-1616	-3.00	3.06	1.11	1.16	387	111
3C 110	FOS H19 B-3	2.16	1.44	-232	14.4	1.80	330	7.4	0.45	733	-0.53	4.14	1.40	1.19	426	112
LBQS 0102-2713	FOS H19 B-3	3.13	1.68	-661	12.2	2.06	-1699	8	0.87	-1268	-2.00	1.38	2.24	2.38	346	75
FBQS J1253175+310550	FOS H19 B-3	7.24	0.65	-396	18.2	1.11	793	4.84	0.27	-262	-2.39	2.87	3.76	2.60	335	66
3C 286	FOS L15 A-1	5.57	1.08	-1757	17.9	0.73	-1000	3.1	0.18	-1131	-1.07	1.77	1.02	1.84	75	12
3C 4543	FOS H27 C-2	2.84	1.44	-556	10.5	0.66	-299	3.46	0.28	-255	-1.30	2.78	0.62	0.78	217	146
3C 4543	FOS H27 A-1	4.22	2.65	-301	19.3	0.56	79	3.16	0.32	20	-1.30	1.59	1.13	1.39	212	141
[HB89] 0107-156	FOS H27 B-3	3.53	2.35	-703	19.1	1.56	-604	3.62	0.27	-1366	-1.30	0.73	1.01	0.96	191	126
[HB89] 1252+119	FOS H27 C-2	6.34	1.56	-734	29.9	0.42	-1778	6.39	0.41	-1002	-1.30	2.24	0.90	0.85	264	155
LBQS 0253-0138	FOS H27 A-1	6.23	1.07	-399	9.48	0.61	-3833	10.8	0.72	-1626	-1.30	2.22	1.21	1.34	267	146
[HB89] 2340-036	FOS H27 C-2	4.52	1.58	205	16.1	1.21	440	9.54	1.12	4967	-1.30	4.37	1.15	1.11	39	7
[HB89] 0954+556	FOS H27 A-1	2.58	1.77	853	8.6	0.70	1782	15.5	0.36	1052	-1.30	0.72	1.21	1.24	268	157
[HB89] 2216-038	FOS H27 A-1	3.25	1.15	-736	10.4	1.88	-341	7.38	0.66	-224	-1.30	1.52	0.84	0.95	261	156
3C 336	FOS H27 B-3	2.36	5.57	148	11.4	2.39	341	6.96	0.95	446	0.56	0.433	1.11	1.27	212	166
TON 0157	FOS H27 B-3	9.8	0.41	2384	16.6	0.61	-3876	8.5	0.14	1969	-2.31	1.7	1.42	1.45	278	177
SBS 1148+549	FOS H27 A-1	4.94	1.31	-1258	13	0.84	-4957	12.6	1.16	-3499	-2.13	5.66	1.28	1.20	279	177
[HB89] 2145+067	FOS H27 C-2	1.81	0.74	1518	11.5	1.70	934	7.18	0.58	1054	-0.20	2.75	0.85	0.71	307	204
[HB89] 0355-483	FOS H27 A-1	4.8	1.51	-1401	17.9	1.08	1935	3.19	0.47	-972	-1.08	2.57	1.24	1.03	270	180
TON 0153	FOS H27 C-2	4.11	0.39	-1527	15.6	0.86	-2517	8.52	0.41	-1782	-1.71	6.18	1.13	0.84	293	183
PG 1254+047	FOS H27 C-2	7.92	1.70	-1409	9.91	1.82	-5922	12.4	2.66	-2503	4.02	1.91	1.30	1.13	308	185
PG 1248+401	FOS H27 B-2	14.6	1.78	-1305	6.84	0.53	-8625	8.91	0.99	-1068	-1.59	2.87	1.32	1.56	290	174

See end of table for explanation of columns.
Continued on next page.

Table 3: Parameters from full-profile fits – continued from previous page.

Name	Inst. Grat. Ap.	$\sigma_{\mathrm{L}\alpha0}$ (Å)	$a_{\mathrm{L}\alpha0}$ (a_{p})	$v_{\mathrm{L}\alpha0}$ (km/s)	$\sigma_{\mathrm{L}\alpha1}$ (Å)	$a_{\mathrm{L}\alpha1}$ (a_{p})	$v_{\mathrm{L}\alpha1}$ (km/s)	σ_{NV} (Å)	a_{NV} (a_{p})	v_{NV} (km/s)	p	a_{p} (flux)	χ^2/ν prof.	χ^2/ν cont.	ν prof.	ν cont.
[HB89] 2230+114	FOS H27 A-1	4.44	2.58	122	17	0.96	792	4.09	0.11	1148	-0.07	1.43	1.21	1.06	315	199
LBQS 1229-0207	FOS H27 C-1	2.3	1.77	-256	10.3	2.66	-447	6.3	0.79	-87	-0.60	1.66	1.16	1.41	196	159
[HB89] 2302+029	FOS H27 B-3	1.04	-0.22	657	16.9	0.20	-4168	21.5	0.43	-2948	-0.27	4.34	1.38	1.59	177	138
SBS 1317+520	FOS H27 A-1	2.69	1.41	-851	12.5	1.47	-101	7.49	0.41	529	-1.84	2.73	1.44	1.48	318	172
[HB89] 1718+481	FOS H27 C-2	3.58	0.66	-413	17.1	0.68	-258	5.98	0.37	-593	-2.01	15.1	0.72	0.66	191	182
[HB89] 0024+224	FOS H27 C-2	6.84	0.99	-1368	10.7	0.91	-3067	14.4	0.60	-2856	-1.13	2.15	0.99	0.64	309	189
PG 1352+011	FOS H27 C-2	2.33	-0.27	1665	14.6	1.13	-1837	11.2	0.55	-2431	-1.48	3.68	0.81	0.76	274	192
PG 1206+459	FOS H27 C-2	5.95	0.33	-748	11.7	1.42	-382	8.69	1.10	-1039	-0.04	4.62	1.19	0.89	222	175
[HB89] 1038+064	FOS H27 B-2	4.68	0.63	-159	12.2	0.73	-2786	11.3	0.64	-1458	-1.59	2.76	1.04	1.30	306	231
PG 1241+176	FOS H27 C-2	2.2	1.36	919	12.5	1.15	2095	3.92	0.61	1074	-0.12	3.59	1.87	1.52	284	210
PG 1008+133	FOS H27 C-2	17.6	0.69	628	22.3	0.08	-5647	6.43	0.20	-644	-1.33	2.96	1.63	1.37	290	237
[HB89] 0454+039	FOS H27 B-3	4.92	1.14	16	10.7	0.89	-2152	11.3	0.74	-762	-1.28	1.78	1.86	1.35	259	188
FBQS J1259487+342322	FOS H27 C-2	2.65	2.51	128	12.3	1.91	-443	6.07	0.86	166	-0.54	1.11	0.90	0.52	353	244
[HB89] 0302-223	FOS H27 B-1	6.36	0.83	-1236	32.4	0.61	-694	7.21	0.31	-2153	-1.30	2.28	2.14	1.87	227	157
[HB89] 0232-042	FOS H27 B-2	4.87	1.17	114	16.7	1.03	-725	6.36	0.39	267	-1.71	2.97	1.84	1.07	378	158
[HB89] 1630+377	FOS H27 B-1	4.05	0.87	-605	14.5	1.14	-983	7.76	0.49	-200	-1.68	3.48	1.33	1.08	338	140
PG 0117+213	FOS H27 B-2	6.83	0.54	-658	20.9	0.85	2026	1.64	0.13	93	-1.06	3.76	1.67	1.71	260	69
[HB89] 0743-673	FOS H27 C-2	3.83	3.99	597	14.2	0.69	-495	8.1	0.34	39	-0.65	1.98	1.19	1.07	285	111

The first two columns give the NED name of the target, plus the HST instrument, grating, and aperture used to take the spectrum. $\sigma_{\mathrm{L}\alpha0}$ is the width of the narrow Lyman-α component (corrected for redshift using the NED value of z, see Table 1). $a_{\mathrm{L}\alpha0}$ is the amplitude of this component, normalized by the continuum flux a_{p}. $v_{\mathrm{L}\alpha0}$ is the shift of the component center from the nominal wavelength calculated with the NED redshift. The next six columns give the same quantities for the broad Lyman-α component (Lα1), and the N V component. p is the continuum power law index, and a_{p} is the continuum flux at the nominal Lyman-α central wavelength, in units of 10^{-15}erg s^{-1} cm^{-2} Å^{-1}. The last columns give the reduced χ^2 value χ^2/ν and the number of degrees of freedom ν for the continuum and line-profile fits.

Table 4: Best-fit spectral parameters from fits to the red side only of the Lyman-α line.

Name	Inst. Grat. Ap.	$\sigma_{L\alpha 0}$ (Å)	$a_{L\alpha 0}$ (a_p)	$v_{L\alpha 0}$ (km/s)	$\sigma_{L\alpha 1}$ (Å)	$a_{L\alpha 1}$ (a_p)	$v_{L\alpha 1}$ (km/s)	σ_{NV} (Å)	a_{NV} (a_p)	v_{NV} (km/s)	p	a_p (flux)	χ^2/ν prof.	χ^2/ν cont.	ν prof.	ν cont.
MRK 0335	FOS H13 B-3	2.46	8.92	0	8.12	2.60	0	5.23	0.97	0	-1.30	77.4	1.24	0.88	199	177
SBS 1626+554	FOS H13 B-3	4.24	1.48	0	20.6	1.41	0	4.71	0.29	0	-1.30	21.8	1.27	1.24	326	217
PG 0026+129	FOS H13 B-3	6.38	3.47	0	2.87	7.31	0	11.8	1.09	0	-1.30	19.6	1.20	1.26	311	199
3C 273	FOS H13 A-1	3.93	0.77	0	12.1	0.74	0	7.88	0.32	0	-1.30	269	0.76	0.79	372	204
3C 273	FOS H13 B-3	3.79	0.96	0	16.5	0.62	0	8.39	0.18	0	-1.30	269	1.14	1.08	354	204
3C 273	FOS H13 B-1	3.92	0.96	0	16.7	0.57	0	7.99	0.19	0	-1.30	282	1.15	1.04	352	203
3C 273	FOS H13 C-2	4.47	0.85	0	17.1	0.56	0	7.71	0.19	0	-1.30	279	1.03	0.88	317	160
3C 273	FOS H13 B-2	4.64	0.76	0	17.2	0.57	0	8.73	0.20	0	-1.30	271	0.83	0.82	355	203
PG 1322+659	FOS H13 B-3	5.11	3.03	0	15.6	0.83	0	6.92	0.78	0	-1.30	9.19	2.63	1.51	279	194
PG 1116+215	FOS H13 C-2	5.11	1.11	0	25.1	0.86	0	4.86	0.25	0	-1.30	53.3	0.88	0.58	362	219
[HB89] 1427+480	FOS H13 B-3	3.53	5.04	0	10	1.75	0	7.31	0.68	0	-1.30	7.89	1.32	1.08	350	110
PG 0953+414	FOS H13 C-2	5.26	2.27	0	22.6	1.20	0	4.09	0.39	0	-1.30	17.1	1.35	0.69	396	110
[HB89] 1156+213	FOS H19 B-3	2.96	4.29	0	17.1	1.43	0	5.59	0.36	0	-1.30	3.15	0.87	0.78	248	156
[HB89] 1425+267	FOS H19 B-3	8.78	2.16	0	28	0.97	0	1.66	0.17	0	-1.30	3.82	1.63	0.90	271	185
HS 0624+6907	FOS H19 B-2	16.5	0.77	0	16.5	1.39	0	5.76	0.76	0	-1.30	15	0.90	0.76	252	133
[HB89] 1543+489	FOS H19 B-3	19.8	0.30	0	19.8	1.30	0	1.24	0.43	0	-1.30	5.55	1.55	0.99	273	149
3C 215	FOS H19 A-1	8.26	4.31	0	22.4	1.18	0	22.1	0.69	0	-1.30	0.779	0.65	0.54	339	197
LBQS 1230+0947	FOS H19 A-1	7.18	2.59	0	7.18	2.99	0	9.81	1.67	0	-1.30	6.02	1.11	1.33	337	175
[HB89] 1049+616	FOS L15 C-1	10	1.21	0	32.3	0.80	0	7.24	0.24	0	-1.30	5.33	0.98	0.68	61	39
[HB89] 2308+098	FOS H19 B-3	4.04	2.30	0	30.8	1.24	0	1.32	0.19	0	-1.30	5.98	0.71	0.57	330	197
PG 0003+158	FOS H19 C-2	4.64	1.93	0	19.5	1.44	0	5.85e+07	0.06	0	-1.30	11.3	1.28	0.51	327	202
FBQS J0745416+314256	FOS H19 C-2	6.21	0.81	0	19.8	1.58	0	5.28	0.09	0	-1.30	5.57	0.84	0.63	350	214
[HB89] 2112+059 NED01	FOS H19 C-2	19.8	0.32	0	19.8	1.25	0	2.53	-0.15	0	-1.30	5.97	0.97	0.59	351	181
SBS 1259+593	FOS H19 C-2	0.368	12.43	0	18.5	0.86	0	0.659	-0.10	0	-1.30	11.1	0.76	0.85	353	216
[HB89] 2128-123	FOS H19 C-2	7.99	1.81	0	30.3	1.22	0	-2.8	0.04	0	-1.30	8.67	1.76	1.88	226	178
[HB89] 0850+440	FOS H19 C-2	3.4	1.75	0	16.2	0.73	0	6.47	0.36	0	-1.30	4.72	0.43	0.59	341	191
FBQS J0958209+322402	FOS H19 C-2	3.98	0.57	0	33.9	0.61	0	1.12	0.15	0	-1.30	4.66	0.32	0.61	337	224
[HB89] 0015+162	FOS H19 B-3	3.19	1.78	0	17.7	1.17	0	6.99	0.49	0	-1.30	0.444	0.98	1.09	346	228
3C 334	FOS H19 C-2	13.3	0.88	0	47.7	0.58	0	22.9	-0.00	0	-1.30	5.05	0.89	1.01	350	227
NGC 2841 UB3	FOS H19 C-2	2.92	0.70	0	17.8	0.94	0	7.63	0.29	0	-1.30	5.9	1.00	0.98	352	211
[HB89] 1136-135	FOS H19 C-2	11	1.32	0	46.8	0.60	0	1.68	0.32	0	-1.30	4.45	1.29	0.92	352	230
[HB89] 0405-123	FOS H19 C-2	5.61	1.68	0	24.3	1.14	0	3.28	0.22	0	-1.30	15.8	1.32	0.86	336	210
[HB89] 0439-433	FOS H19 C-2	5.37	2.03	0	27.2	1.00	0	2.7	0.18	0	-1.30	3.53	1.39	0.86	340	224

See end of table for explanation of columns.
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Table 4: Parameters from red-side-only fits – continued from previous page.

Name	Inst. Grat. Ap.	$\sigma_{L\alpha 0}$ (Å)	$a_{L\alpha 0}$ (a_p)	$v_{L\alpha 0}$ (km/s)	$\sigma_{L\alpha 1}$ (Å)	$a_{L\alpha 1}$ (a_p)	$v_{L\alpha 1}$ (km/s)	σ_{NV} (Å)	a_{NV} (a_p)	v_{NV} (km/s)	p	a_p (flux)	χ^2/ν prof.	χ^2/ν cont.	ν prof.	ν cont.
FBQS J1010275+413238	FOS H19 C-2	5.08	2.90	0	26.9	1.46	0	3.99	0.37	0	-1.30	6.32	2.09	1.46	338	200
3C 095	FOS H19 C-2	12.4	0.75	0	36	0.55	0	2.28	0.10	0	-1.30	9.19	0.96	1.05	355	237
PG 0044+030	FOS H19 C-2	2.69	2.53	0	21.1	1.68	0	9.8	0.28	0	-1.30	3.68	0.69	0.62	390	238
[HB89] 2243-123	FOS H19 C-2	3.97	1.02	0	22.4	1.23	0	4.38	-0.02	0	-1.30	4.41	1.69	0.88	392	239
[HB89] 1104+167	FOS H19 C-2	5.27	1.23	0	20.3	1.67	0	5.22	0.04	0	-1.30	7.95	1.22	1.22	365	239
3C 263	FOS H19 A-1	6.34	1.87	0	22	1.12	0	3.31	0.35	0	-1.30	6.16	1.22	1.16	395	242
3C 263	FOS H19 C-2	6.09	1.32	0	26.6	1.01	0	3.37	-0.21	0	-1.30	7.06	1.68	0.68	374	240
3C 057	FOS H19 B-2	6.63	1.22	0	18.6	0.27	0	6.5	0.45	0	-1.30	6.9	2.53	1.37	376	235
[HB89] 2344+092	FOS H19 C-2	2.94	1.48	0	16.9	1.29	0	5.78	0.31	0	-1.30	3.62	1.42	1.23	347	237
[HB89] 0923+392	FOS H19 A-1	6.99	2.60	0	15.4	0.90	0	9.03	0.47	0	-1.30	4.79	0.97	1.00	385	189
[HB89] 2352-342	FOS H19 C-2	9.04	2.88	0	28.5	0.33	0	8.17	0.62	0	-1.30	4.46	1.97	0.90	339	227
[HB89] 1354+195	FOS H19 C-2	4.72	2.16	0	21.1	1.24	0	3.43	0.20	0	-1.30	3.55	1.54	0.89	414	160
[HB89] 1637+574	FOS H19 A-1	4.55	1.60	0	13.7	0.92	0	7.28	0.50	0	-1.30	3	1.16	0.87	422	128
[HB89] 1538+477	FOS H19 C-2	7.39	1.99	0	20.3	1.09	0	7.37	0.30	0	-1.30	5.89	2.42	1.80	288	112
2MASSI J1003067+681316	FOS H19 C-2	0.469	14.27	0	18.5	0.64	0	13.1	0.51	0	-1.30	2.78	1.11	1.16	387	111
3C 110	FOS H19 B-3	6.17	0.74	0	20.4	1.27	0	9.27	0.21	0	-1.30	4.32	1.40	1.19	426	112
LBQS 0102-2713	FOS H19 B-3	1.74	6.46	0	17.2	1.49	0	8	0.40	0	-1.30	1.33	2.24	2.38	346	75
FBQS J1253175+310550	FOS H19 B-3	5.52	0.36	0	18	1.52	0	5.43	0.33	0	-1.30	2.68	3.76	2.60	335	66
3C 286	FOS L15 A-1	3.54	0.18	0	15.7	0.69	0	5.52	0.08	0	-1.30	1.79	1.02	1.84	75	12
3C 4543	FOS H27 C-2	-0.211	-20.86	0	11	0.60	0	3.16	0.26	0	-1.30	2.78	0.62	0.78	217	146
3C 4543	FOS H27 A-1	3.87	2.00	0	19.9	0.56	0	3.04	0.32	0	-1.30	1.59	1.13	1.39	212	141
[HB89] 0107-156	FOS H27 B-3	1.6	10.95	0	17.3	1.60	0	7.44	0.10	0	-1.30	0.73	1.01	0.96	191	126
[HB89] 1252+119	FOS H27 C-2	3.48	0.74	0	17.2	0.79	0	5.96	0.30	0	-1.30	2.24	0.90	0.85	264	155
LBQS 0253-0138	FOS H27 A-1	2.25	2.86	0	18	0.80	0	9.04	0.28	0	-1.30	2.22	1.21	1.34	267	146
[HB89] 2340-036	FOS H27 C-2	6.62	1.90	0	30.6	0.81	0	1.07	-0.34	0	-1.30	4.37	1.15	1.11	39	7
[HB89] 0954+556	FOS H27 A-1	4.21	2.95	0	25.7	0.80	0	5.57	-0.05	0	-1.30	0.72	1.21	1.24	268	157
[HB89] 2216-038	FOS H27 A-1	6.72	0.83	0	14.2	1.06	0	6.84	0.50	0	-1.30	1.52	0.84	0.95	261	156
3C 336	FOS H27 B-3	5.29	1.60	0	23.5	1.25	0	1.47	0.22	0	-1.30	0.512	1.11	1.27	212	166
TON 0157	FOS H27 B-3	-1.19	-125.44	0	12.4	0.82	0	14.1	0.24	0	-1.30	1.55	1.42	1.45	278	177
SBS 1148+549	FOS H27 A-1	6.08	-0.03	0	19.1	1.66	0	25.5	-0.00	0	-1.30	5.23	1.28	1.20	279	177
[HB89] 2145+067	FOS H27 C-2	2.93	10.51	0	9.5	1.80	0	11.9	0.60	0	-1.30	3.03	0.85	0.71	307	204
[HB89] 0355-483	FOS H27 A-1	1.76	4.44	0	18.4	1.16	0	7.46	0.28	0	-1.30	2.63	1.24	1.03	270	180
TON 0153	FOS H27 C-2	-13	-349.20	0	13	349.86	0	2	-0.06	0	-1.30	5.96	1.13	0.84	293	183
PG 1254+047	FOS H27 C-2	0.508	11.74	0	19.2	1.26	0	2.02	0.22	0	-1.30	3.25	1.30	1.13	308	185
PG 1248+401	FOS H27 B-2	16.6	0.81	0	16.6	1.29	0	6.33	0.47	0	-1.30	2.78	1.32	1.56	290	174

See end of table for explanation of columns.
Continued on next page.

Table 4: Parameters from red-side-only fits – continued from previous page.

Name	Inst. Grat. Ap.	$\sigma_{L\alpha0}$ (Å)	$a_{L\alpha0}$ (a_p)	$v_{L\alpha0}$ (km/s)	$\sigma_{L\alpha1}$ (Å)	$a_{L\alpha1}$ (a_p)	$v_{L\alpha1}$ (km/s)	σ_{NV} (Å)	a_{NV} (a_p)	v_{NV} (km/s)	p	a_p (flux)	χ^2/ν prof.	χ^2/ν cont.	ν prof.	ν cont.
[HB89] 2230+114	FOS H27 A-1	2.9	2.00	0	8.99	1.87	0	7.67	0.34	0	-1.30	1.58	1.21	1.06	315	199
LBQS 1229-0207	FOS H27 C-1	6.68	1.69	0	26.5	0.75	0	4.04	0.27	0	-1.30	1.78	1.16	1.41	196	159
[HB89] 2302+029	FOS H27 B-3	1.69	1.32	0	18.9	0.31	0	12.9	0.15	0	-1.30	4.8	1.38	1.59	177	138
SBS 1317+520	FOS H27 A-1	5.21	0.88	0	23.9	0.96	0	1.83e+07	0.05	0	-1.30	2.63	1.44	1.48	318	172
[HB89] 1718+481	FOS H27 C-2	2.6	0.58	0	17.7	0.78	0	7.65	0.33	0	-1.30	14.2	0.72	0.66	191	182
[HB89] 0024+224	FOS H27 C-2	4.1	0.62	0	18.6	0.80	0	8.91	0.10	0	-1.30	2.18	0.99	0.64	309	189
PG 1352+011	FOS H27 C-2	0.612	8.35	0	18.4	1.22	0	0.0918	-0.07	0	-1.30	3.61	0.81	0.76	274	192
PG 1206+459	FOS H27 C-2	0.693	11.64	0	17	1.42	0	5.9	0.47	0	-1.30	5.16	1.19	0.89	222	175
[HB89] 1038+064	FOS H27 B-2	3.84	0.44	0	17.4	0.78	0	7.76	0.33	0	-1.30	2.68	1.04	1.30	306	231
PG 1241+176	FOS H27 C-2	4.42	-0.26	0	7.17	1.54	0	17.7	0.64	0	-1.30	4.01	1.87	1.52	284	210
PG 1008+133	FOS H27 C-2	1.54	3.58	0	16.6	0.87	0	6.83	0.23	0	-1.30	2.93	1.63	1.37	290	237
[HB89] 0454+039	FOS H27 B-3	4.17	1.22	0	29.1	0.72	0	6.15	0.20	0	-1.30	1.8	1.86	1.35	259	188
FBQS J1259487+342322	FOS H27 C-2	4.61	1.89	0	24.4	0.95	0	3.91	0.36	0	-1.30	1.19	0.90	0.52	353	244
[HB89] 0302-223	FOS H27 B-1	1.25	10.20	0	24	0.93	0	7.22	0.04	0	-1.30	2.28	2.14	1.87	227	157
[HB89] 0232-042	FOS H27 B-2	6.21	1.54	0	19.8	0.65	0	6.8	0.38	0	-1.30	2.89	1.84	1.07	378	158
[HB89] 1630+377	FOS H27 B-1	1.82	7.86	0	19.8	0.94	0	5.79	0.25	0	-1.30	3.4	1.33	1.08	338	140
PG 0117+213	FOS H27 B-2	1.57	22.69	0	23.5	0.92	0	6.24	0.16	0	-1.30	3.82	1.67	1.71	260	69
[HB89] 0743-673	FOS H27 C-2	3.52	1.14	0	8.73	1.42	0	7.32	0.38	0	-1.30	2.05	1.19	1.07	285	111

The first two columns give the NED name of the target, plus the HST instrument, grating, and aperture used to take the spectrum. $\sigma_{L\alpha0}$ is the width of the narrow Lyman-α component (corrected for redshift using the NED value of z, see Table 1). $a_{L\alpha0}$ is the amplitude of this component, normalized by the continuum flux a_p. $v_{L\alpha0}$ is the shift of the component center from the nominal wavelength calculated with the NED redshift. The next six columns give the same quantities for the broad Lyman-α component (Lα1), and the N V component. p is the continuum power law index, and a_p is the continuum flux at the nominal Lyman-α central wavelength, in units of 10^{-15}erg s^{-1} cm^{-2} Å^{-1}. The last columns give the reduced χ^2 value χ^2/ν and the number of degrees of freedom ν for the continuum and line-profile fits.